

## Second and Higher Order Linear Differential Equations

Larry Caretto  
Mechanical Engineering 501AB  
**Seminar in Engineering Analysis**

October 9, 2017

California State University  
**Northridge**

## Outline

- Review last class and homework
- Apply material from last class to mechanical vibrations
- Higher order equations with constant coefficients
  - Homogenous and nonhomogenous solutions
- Existence and uniqueness of solutions for higher order equations

California State University  
**Northridge**

2

## Review Undetermined Coefficients

- Used for constant coefficient equation  $y'' + ay' + by = r(x)$
- Solution is  $y = y_p + y_H$ , where  $y_H$  is solution of  $y_H'' + ay_H' + by = 0$
- Postulate a solution for  $y_p$  following guidelines on next two charts
- Plug solution into ODE and solve for unknown coefficients
  - Overall coefficients of like terms on both sides of ODE must vanish

California State University  
**Northridge**

3

## Table of Trial $y_p$ Solutions

For these $r(x)$	Start with this $y_p$
$r(x) = Ae^{ax}$	$y_p = Be^{ax}$
$r(x) = Ax^n$	$y_p = a_0 + a_1x + \dots + a_nx^n$
$r(x) = A\sin \omega t$	$y_p = B \sin \omega t + C \cos \omega t$
$r(x) = A\cos \omega t$	
$r(x) = Ae^{ax}\sin \omega t$	$y_p = e^{ax} (B \sin \omega t + C \cos \omega t)$
$r(x) = Ae^{ax}\cos \omega t$	

California State University  
**Northridge**

4

## Special Rules

- If the right-hand-side,  $r(x)$  consists of more than one term from the previous table, use a  $y_p$  that contains all the corresponding  $y_p$  terms
  - For  $r(x) = A\cos bx + Ce^{dx}$ , use  $y_p = E \sin bx + F \cos bx + Ge^{dx}$
- If  $r(x)$  is proportional to a solution for the homogenous equation, use  $y_p$  equal to  $x$  times the  $y_p$  shown in the table
  - For a double root, multiply table  $y_p$  by  $x^2$

California State University  
**Northridge**

5

## Review Parameter Variation

- Want to solve linear equation
 
$$\frac{d^2y}{dx^2} + p(x)\frac{dy}{dx} + q(x)y = r(x)$$
- Have to solve homogenous equation to get two (LI) solutions  $y_1$  and  $y_2$
- Define  $W$  from these two solutions

$$W = y_1 \frac{dy_2}{dx} - y_2 \frac{dy_1}{dx}$$

California State University  
**Northridge**

6

### Review Parameter Variation II

- Define  $u(x)$  and  $v(x)$  such that  $y_p = y_1 u + y_2 v$ , where  $u$  and  $v$  are found from the following integrals

$$u = -\int \frac{y_2 r(x)}{W(x)} dx \quad v = \int \frac{y_1 r(x)}{W(x)} dx$$

$$y_p = y_1 u + y_2 v = -y_1 \int \frac{y_2 r(x)}{W(x)} dx + y_2 \int \frac{y_1 r(x)}{W(x)} dx$$

- Get  $y = y_H + y_p$  and evaluate constants in  $y_H$  solution from initial conditions

### Nonhomogenous Summary

- Undetermined coefficients is simpler approach but is limited
  - Constant coefficient equations
  - Limited set of functions
- Variation of parameters is more complex, but handles more cases
- In reality, there are no general methods to get homogenous solution to linear, second-order ODE without constant coefficients

### Higher Order Equations

- General  $n^{\text{th}}$  order linear equation
- $$\frac{d^n y}{dx^n} + p_{n-1}(x) \frac{d^{n-1} y}{dx^{n-1}} + \dots + p_1(x) \frac{dy}{dx} + p_0(x) y = r(x)$$
- Treatment similar to second order
  - Look at homogenous solution first
  - Combine with particular solution
  - Must consider ODE with constant coefficients to get any general results
    - This is similar to second order

### Higher Order Equations II

- Look at general  $n^{\text{th}}$  order differential equation with constant coefficients

$$\frac{d^n y}{dx^n} + a_{n-1} \frac{d^{n-1} y}{dx^{n-1}} + \dots + a_1 \frac{dy}{dx} + a_0 y = r(x)$$

- Find  $y_H$  from homogenous ODE

$$\frac{d^n y_H}{dx^n} + a_{n-1} \frac{d^{n-1} y_H}{dx^{n-1}} + \dots + a_1 \frac{dy_H}{dx} + a_0 y_H = 0$$

- Homogenous solution  $y_H = \sum_{k=1}^n C_k e^{\lambda_k x}$

### Higher Order Equations III

- Homogenous solution  $y_H = \sum_{k=1}^n C_k e^{\lambda_k x}$
- In homogenous solution, the values of  $\lambda_k$  are solutions to the equation  $\lambda^n + a_{n-1} \lambda^{n-1} + a_{n-2} \lambda^{n-2} + \dots + a_1 \lambda + a_0 = 0$
- Complex solutions occur as complex conjugates giving sines and cosines
- For double roots  $\lambda_k = \text{DR}$ , we modify solution to give  $(C_k + C_{k+1} x) e^{(\text{DR})x}$

### Higher Order Equations IV

- For nonhomogenous equations we can find the total solution  $y = y_H + y_p$
- $y_p$  may be found by undetermined coefficients or variation of parameters
  - Use same process for method of undetermined coefficients
  - Variation of parameters is more complex since it involves solution of simultaneous equations for new solutions

### Higher Order Equations V

- There are n linearly-independent solutions to a linear, homogenous n<sup>th</sup> order ODE
- The n linearly-independent solutions form a basis for all solutions
  - Use same process for method of undetermined coefficients
  - Variation of parameters is more complex since it involves solution of simultaneous equations for new solutions

### Existence and Uniqueness

- General linear, homogenous, n<sup>th</sup> order ODEs have a unique solution over a < x < b if all the p<sub>k</sub>(x) are continuous there

$$\frac{d^n y}{dx^n} + p_{n-1}(x) \frac{d^{n-1} y}{dx^{n-1}} + \dots + p_1(x) \frac{dy}{dx} + p_0(x)y = 0$$

- The proposed solutions y<sub>k</sub>(x) to the homogenous ODE are linearly independent if the Wronskian (see next chart) is nonzero

### Wronski Determinant

- Wronskian, W, for nth order ODE (with notation that y<sup>(k)</sup> denotes d<sup>k</sup>y/dx<sup>k</sup>)

$$W = \begin{vmatrix} y_1 & y_2 & y_3 & \dots & \dots & y_n \\ y_1^{(1)} & y_2^{(1)} & y_3^{(1)} & \dots & \dots & y_n^{(1)} \\ y_1^{(2)} & y_2^{(2)} & y_3^{(2)} & \dots & \dots & y_n^{(2)} \\ \vdots & \vdots & \vdots & \ddots & & \vdots \\ \vdots & \vdots & \vdots & & \ddots & \vdots \\ y_1^{(n)} & y_2^{(n)} & y_3^{(n)} & \dots & \dots & y_n^{(n)} \end{vmatrix}$$

### Application: Structural Member

- An elastic beam with an applied load, f(x), per unit length, in the y direction (normal to the beam)
  - Beam is bent under this load
  - Bending moment, M(x) is given by second-order ODE: d<sup>2</sup>M/dx<sup>2</sup> = f(x)
  - Final deflection is d<sup>2</sup>y/dx<sup>2</sup>
  - M = EI d<sup>2</sup>y/dx<sup>2</sup> where E is Young's modulus and I is moment of inertia

### Structural Member ODE

- Combine d<sup>2</sup>M/dx<sup>2</sup> = f(x) and M = EI d<sup>2</sup>y/dx<sup>2</sup> to get **EI d<sup>4</sup>y/dx<sup>4</sup> = f(x)**
  - SI units for these quantities are meters for x and y, N/m<sup>2</sup> for E, m<sup>4</sup> for I, N/m for f(x), and N·m for M
  - dimensions for n<sup>th</sup> order derivative are dimensions of numerator divided by (denominator dimensions)<sup>n</sup>
  - Have a total of four boundary conditions at x = 0 and x = L
  - Equation has separable solution

### Solving the Equation

$$\frac{d^4 y}{dx^4} = \frac{f(x)}{EI} \Rightarrow \frac{d^3 y}{dx^3} = \frac{1}{EI} \int f(x) dx + C_1$$

$$\frac{d^2 y}{dx^2} = \frac{1}{EI} \int \left( \int f(x) dx \right) dx + C_1 x + C_2$$

$$\frac{dy}{dx} = \frac{1}{EI} \int \left[ \int \left( \int f(x) dx \right) dx \right] dx + C_1 x^2 + C_2 x + C_3$$

$$\frac{dy}{dx} = \frac{1}{EI} \int \left\{ \int \left[ \int \left( \int f(x) dx \right) dx \right] dx \right\} dx + C_1 x^3 + C_2 x^2 + C_3 x + C_4$$

- Apply boundary conditions to find constants of integration

### Application: Forced Vibrations

- Last week we showed solutions for free vibrations of spring-mass-damper system
- ODE was  $md^2y/dt^2 + cdy/dt + ky = 0$
- Imposed force gives nonhomogenous ODE  $md^2y/dt^2 + cdy/dt + ky = f(t)$
- Consider example where  $f(t) = F_0 \cos \omega t$
- Undetermined coefficient trial solution is  $y_p = A \sin \omega t + B \cos \omega t$

### Forced Vibrations II

- Derivatives of  $y_p = A \sin \omega t + B \cos \omega t$
- $y_p' = \omega A \cos \omega t - \omega B \sin \omega t$
- $y_p'' = -\omega^2 A \sin \omega t - \omega^2 B \cos \omega t$
- Substitute into ODE:  $md^2y/dt^2 + cdy/dt + ky = F_0 \cos \omega t$
- $m[-\omega^2 A \sin \omega t - \omega^2 B \cos \omega t]$   
 $+ c[\omega A \cos \omega t - \omega B \sin \omega t]$   
 $+ k[A \sin \omega t + B \cos \omega t] = F_0 \cos \omega t$

### Forced Vibrations III

- Rearrange to collect sines and cosines
- $m[-\omega^2 A \sin \omega t - \omega^2 B \cos \omega t]$   
 $+ c[\omega A \cos \omega t - \omega B \sin \omega t]$   
 $+ k[A \sin \omega t + B \cos \omega t] = F_0 \cos \omega t$
- $[-m\omega^2 A - c\omega B + kA] \sin \omega t +$   
 $[-m\omega^2 B + c\omega A + kB] \cos \omega t = F_0 \cos \omega t$
- Equate coefficients of sine and cosine terms on both sides of the equation

### Forced Vibrations IV

- $[-m\omega^2 A - c\omega B + kA] \sin \omega t + [-m\omega^2 B + c\omega A + kB] \cos \omega t = F_0 \cos \omega t$
- $(-m\omega^2 + k)A - c\omega B = 0$  (sine terms)
- $c\omega A - (m\omega^2 + k)B = F_0$  (cosines)
- Cramer's rule solution gives

$$A = \frac{\begin{vmatrix} 0 & -c\omega \\ F_0 & k - m\omega^2 \end{vmatrix}}{\begin{vmatrix} k - m\omega^2 & -c\omega \\ c\omega & k - m\omega^2 \end{vmatrix}} \quad B = \frac{\begin{vmatrix} k - m\omega^2 & 0 \\ c\omega & F_0 \end{vmatrix}}{\begin{vmatrix} k - m\omega^2 & -c\omega \\ c\omega & k - m\omega^2 \end{vmatrix}}$$

### Define $\omega_0^2 = k/m$ in Solution

$$A = \frac{\begin{vmatrix} 0 & -c\omega \\ F_0 & k - m\omega^2 \end{vmatrix}}{\begin{vmatrix} k - m\omega^2 & -c\omega \\ c\omega & k - m\omega^2 \end{vmatrix}} \quad B = \frac{\begin{vmatrix} k - m\omega^2 & 0 \\ c\omega & F_0 \end{vmatrix}}{\begin{vmatrix} k - m\omega^2 & -c\omega \\ c\omega & k - m\omega^2 \end{vmatrix}}$$

$$A = \frac{F_0 c \omega}{(k - m\omega^2)^2 + \omega^2 c^2} \quad B = \frac{F_0 (k - m\omega^2)}{(k - m\omega^2)^2 + \omega^2 c^2}$$

$$A = \frac{F_0 c \omega}{m^2 (\omega_0^2 - \omega^2)^2 + \omega^2 c^2} \quad B = \frac{m F_0 (\omega_0^2 - \omega^2)}{m^2 (\omega_0^2 - \omega^2)^2 + \omega^2 c^2}$$

### Undamped Case, $c = 0$

$$A = \frac{F_0 c \omega}{m^2 (\omega_0^2 - \omega^2)^2 + \omega^2 c^2} = 0$$

$$B = \frac{m F_0 (\omega_0^2 - \omega^2)}{m^2 (\omega_0^2 - \omega^2)^2 + \omega^2 c^2} = \frac{m F_0 (\omega_0^2 - \omega^2)}{m^2 (\omega_0^2 - \omega^2)^2} = \frac{F_0}{m(\omega_0^2 - \omega^2)}$$

- $y_p = A \sin \omega t + B \cos \omega t = \frac{F_0}{m(\omega_0^2 - \omega^2)} \cos \omega t$
- From last week,  $y_H = C \sin \omega_0 t + D \cos \omega_0 t = E \cos(\omega_0 t + \delta)$
- Look at initial conditions

### Undamped Case II

---

$y = y_H + y_P = C \sin \omega_0 t + D \cos \omega_0 t + \frac{F_0}{m(\omega_0^2 - \omega^2)} \cos \omega t$

- Initial conditions  $y(0) = y_0$  and  $y'(0) = v_0$
- $y_0 = D + F_0/m/(\omega_0^2 - \omega^2)$
- $v_0 = \omega_0 C$

$$y = \frac{v_0}{\omega_0} \sin \omega_0 t + \left[ y_0 - \frac{F_0}{m(\omega_0^2 - \omega^2)} \right] \cos \omega_0 t + \frac{F_0}{m(\omega_0^2 - \omega^2)} \cos \omega t$$

$$\frac{y}{y_0} = \frac{v_0}{\omega_0 y_0} \sin \omega_0 t + \left[ 1 - \frac{F_0}{m y_0 (\omega_0^2 - \omega^2)} \right] \cos \omega_0 t + \frac{F_0}{m y_0 (\omega_0^2 - \omega^2)} \cos \left( \frac{\omega}{\omega_0} \omega_0 t \right)$$

California State University Northridge 25

### Undamped Case III

---


$$\frac{F_0}{m y_0 (\omega_0^2 - \omega^2)} = \frac{F_0}{m y_0 \omega_0^2 \left[ 1 - \left( \frac{\omega}{\omega_0} \right)^2 \right]} = \frac{F_0}{m y_0 \frac{k}{m} \left[ 1 - \left( \frac{\omega}{\omega_0} \right)^2 \right]}$$

$$\frac{y}{y_0} = \frac{v_0}{\omega_0 y_0} \sin \omega_0 t + \left[ 1 - \frac{F_0/k y_0}{1 - \omega^2/\omega_0^2} \right] \cos \omega_0 t + \frac{F_0/k y_0}{1 - \omega^2/\omega_0^2} \cos \left( \frac{\omega}{\omega_0} \omega_0 t \right)$$

- $y/y_0$  is a function of  $\omega_0 t$  and the following three (dimensionless) parameters:  
 $v_0/\omega_0 y_0$ ,  $F_0/k y_0$  and  $\omega/\omega_0$

California State University Northridge 26

### Undamped Case IV

---

- Start with solution below and convert  $\omega_0 t$  sine and cosine terms to a cosine term

$$y = A \sin \omega_0 t + B \cos \omega_0 t + \frac{F_0}{m(\omega_0^2 - \omega^2)} \cos \omega t$$

$$A = \frac{v_0}{\omega_0} \quad B = y_0 - \frac{F_0}{m(\omega_0^2 - \omega^2)}$$

$$y = C \cos(\omega_0 t - \delta) + \frac{F_0}{m(\omega_0^2 - \omega^2)} \cos \omega t \quad \delta = \tan^{-1} \left( \frac{A}{B} \right)$$

$$C = \sqrt{A^2 + B^2} = \sqrt{\left( \frac{v_0}{\omega_0} \right)^2 + \left( y_0 - \frac{F_0}{m(\omega_0^2 - \omega^2)} \right)^2}$$

California State University Northridge 27

### Undamped Case V

---

- Compute dimensionless C and  $\delta$

$$\frac{C}{y_0} = \sqrt{\left( \frac{v_0}{y_0 \omega_0} \right)^2 + \left( 1 - \frac{F_0}{y_0 m (\omega_0^2 - \omega^2)} \right)^2}$$

$$\delta = \tan^{-1} \left( \frac{A}{B} \right) = \tan^{-1} \left( \frac{\frac{v_0}{\omega_0}}{y_0 - \frac{F_0}{m(\omega_0^2 - \omega^2)}} \right) = \tan^{-1} \left( \frac{\frac{v_0}{y_0 \omega_0}}{1 - \frac{F_0}{m y_0 (\omega_0^2 - \omega^2)}} \right)$$

$$\frac{y}{y_0} = \frac{C}{y_0} \cos(\omega_0 t - \delta) + \frac{F_0}{y_0 m (\omega_0^2 - \omega^2)} \cos \omega t$$

California State University Northridge 28

### Undamped Case VI

---

- $y/y_0$  is a function of  $\omega_0 t$ ,  $v_0/\omega_0 y_0$ ,  $F_0/k y_0$ , and  $\omega/\omega_0$

$$\frac{F_0}{m y_0 (\omega_0^2 - \omega^2)} = \frac{F_0/k y_0}{1 - \left( \frac{\omega}{\omega_0} \right)^2}$$

$$\frac{C}{y_0} = \sqrt{\left( \frac{v_0}{y_0 \omega_0} \right)^2 + \left( 1 - \frac{F_0/k y_0}{1 - \left( \frac{\omega}{\omega_0} \right)^2} \right)^2}$$

$$\tan \delta = \frac{\frac{v_0}{y_0 \omega_0}}{1 - \frac{F_0/k y_0}{1 - \left( \frac{\omega}{\omega_0} \right)^2}}$$

$$\frac{y}{y_0} = \frac{C}{y_0} \cos(\omega_0 t - \delta) + \frac{F_0/k y_0}{1 - \left( \frac{\omega}{\omega_0} \right)^2} \cos \left( \frac{\omega}{\omega_0} \omega_0 t \right)$$

California State University Northridge 29

### Zero Initial Conditions

---

- Without forcing ( $F_0 = 0$ ), when  $y_0 = v_0 = 0$ , the solution is  $y = 0$  for all  $t$
- Forcing gives a nonzero solution
- Start with general solution for  $c = 0$

$$y = y_H + y_P = C \sin \omega_0 t + D \cos \omega_0 t + \frac{F_0}{m(\omega_0^2 - \omega^2)} \cos \omega t$$

- $v_0 = y'(0) = 0$  gives  $C = 0$
- $y_0 = y(0) = 0$  gives  $D = -F_0/m/(\omega_0^2 - \omega^2)$

$$y = \frac{F_0}{m(\omega_0^2 - \omega^2)} (\cos \omega t - \cos \omega_0 t)$$

California State University Northridge 30

### Zero Initial Conditions II

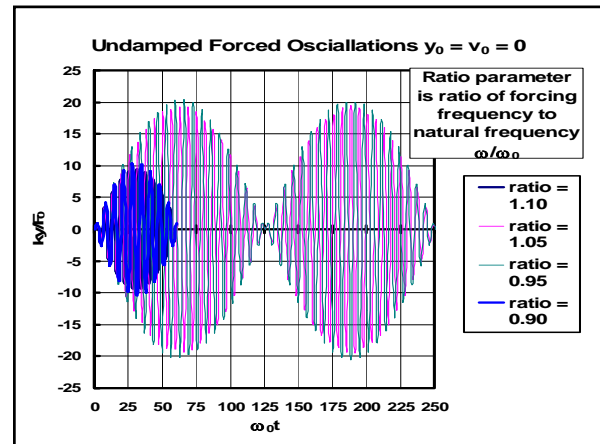
- Rearrange solution for  $c = y_0 = v_0 = 0$

$$y = \frac{F_0}{m\omega_0^2(1 - \omega^2/\omega_0^2)} \left[ \cos\left(\frac{\omega}{\omega_0}\omega_0 t\right) - \cos\omega_0 t \right]$$

$$\frac{ym\omega_0^2}{F_0} = \frac{ym}{F_0} \frac{k}{m} = \frac{yk}{F_0} = \frac{1}{(1 - \omega^2/\omega_0^2)} \left[ \cos\left(\frac{\omega}{\omega_0}\omega_0 t\right) - \cos\omega_0 t \right]$$

- Plot  $yk/F_0$  versus  $\omega_0 t$  with  $\omega/\omega_0$  as a parameter

California State University Northridge 31



### Resonance Condition

- Current equation for  $y/y_0$  has several terms with  $1 - \omega^2/\omega_0^2$  in denominator
- Solution is not valid when  $\omega = \omega_0$
- If  $\omega = \omega_0$ ,  $r(x) = F_0 \cos \omega t$  is proportional to homogenous equation solution
- Have to get new particular solution
- Use undetermined coefficients approach starting with  $y_p = t[A \sin \omega t + B \cos \omega t]$

California State University Northridge 33

### $c = 0$ Resonance Solution II

- Remember  $\omega = \omega_0 = (k/m)^{1/2}$  here
- Derivatives of  $y_p = t[A \sin \omega t + B \cos \omega t]$
- $y_p' = t[\omega A \cos \omega t - \omega B \sin \omega t] + A \sin \omega t + B \cos \omega t$
- $y_p'' = t[-\omega^2 A \sin \omega t - \omega^2 B \cos \omega t] + 2\omega A \cos \omega t - 2\omega B \sin \omega t$
- Substitute into ODE for  $c = 0$  and  $m = k\omega^2$ :  $m d^2 y_p / dt^2 + k y_p = m d^2 y_p / dt^2 + m \omega^2 y_p = F_0 \cos \omega t$

California State University Northridge 34

### $c = 0$ Resonance Solution III

- $m t [-\omega^2 A \sin \omega t - \omega^2 B \cos \omega t] + m [2\omega A \cos \omega t - 2\omega B \sin \omega t] + m \omega^2 t [A \sin \omega t + B \cos \omega t] = F_0 \cos \omega t$
- After cancellations we have  $m [2\omega A \cos \omega t - 2\omega B \sin \omega t] = F_0 \cos \omega t$
- This gives  $B = 0$  and  $A = F_0 / 2m\omega$
- $y_p = [F_0 / 2m\omega] t \sin \omega t$
- Particular solution increases without bound as  $t$  increases

California State University Northridge 35

### Examine Damping

- Damped oscillations without external force
  - derived (homogenous equation) solutions last week
  - Three cases: underdamping, critical damping, and overdamping
  - All cases show  $y$  goes to zero as  $t$  increases
  - Look at particular solution only to show effect of forced oscillations
  - Effects come from amplitude of oscillations

California State University Northridge 36

### General Case for $c \neq 0$

- Convert  $y_p = C \sin \omega t + D \cos \omega t = E \cos(\omega t - \delta)$  to examine amplitude
- $C^2 + D^2 = E^2$  and  $\delta = \tan^{-1}(C/D)$
- Apply this to write  $y_p = E \cos(\omega t - \delta)$

$$y_p = \frac{F_0 \omega c \sin \omega t}{m^2(\omega_0^2 - \omega^2)^2 + \omega^2 c^2} + \frac{F_0 m(\omega_0^2 - \omega^2) \cos \omega t}{m^2(\omega_0^2 - \omega^2)^2 + \omega^2 c^2}$$

$$\delta = \tan^{-1} \left( \frac{\omega c F_0}{m^2(\omega_0^2 - \omega^2)^2 + \omega^2 c^2} / \frac{F_0 m(\omega_0^2 - \omega^2)}{m^2(\omega_0^2 - \omega^2)^2 + \omega^2 c^2} \right) = \tan^{-1} \left( \frac{\omega c}{m(\omega_0^2 - \omega^2)} \right)$$

California State University Northridge 37

### Find $\omega$ that Maximizes C

$$C = \sqrt{\left( \frac{F_0 \omega c}{m^2(\omega_0^2 - \omega^2)^2 + \omega^2 c^2} \right)^2 + \left( \frac{F_0 m(\omega_0^2 - \omega^2)}{m^2(\omega_0^2 - \omega^2)^2 + \omega^2 c^2} \right)^2}$$

$$= F_0 \sqrt{\frac{\omega^2 c^2 + m^2(\omega_0^2 - \omega^2)^2}{[m^2(\omega_0^2 - \omega^2)^2 + \omega^2 c^2]^2}} = \frac{F_0}{\sqrt{m^2(\omega_0^2 - \omega^2)^2 + \omega^2 c^2}}$$

$$\frac{dC}{d\omega} = \frac{-F_0 [m^2 2(\omega_0^2 - \omega^2)(-2\omega) + 2\omega c^2]}{2 [m^2(\omega_0^2 - \omega^2)^2 + \omega^2 c^2]^{3/2}} = 0$$

$$m^2 2(\omega_0^2 - \omega^2)(-2\omega) + 2\omega c^2 = \omega [-4m^2(\omega_0^2 - \omega^2) + 2c^2] = 0$$

$$c^2 = 2m^2(\omega_0^2 - \omega^2)$$

California State University Northridge 38

### Amplitude of $y_p$ versus $\omega$

$$c^2 = 2m^2(\omega_0^2 - \omega^2) \Rightarrow \omega^2 = \omega_0^2 - \frac{c^2}{2m^2}$$

- Maximum amplitude equation not valid if  $c^2/2m^2 > \omega_0^2 = k/m$
- Look at behavior of  $y_p = C \cos(\omega t - \delta)$  by examining C versus  $\omega$
- Write dimensionless equation for C, which has dimensions of length

$$\frac{m\omega_0^2}{F_0} C = \frac{m\omega_0^2}{F_0} \frac{F_0}{\sqrt{m^2(\omega_0^2 - \omega^2)^2 + \omega^2 c^2}}$$

California State University Northridge 39

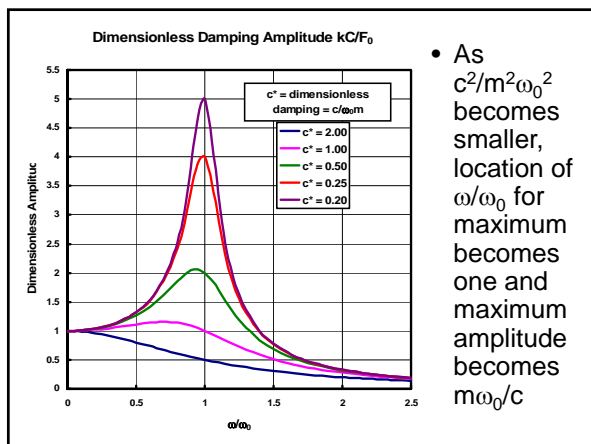
### Amplitude of $y_p$ versus $\omega$ II

$$\frac{m\omega_0^2}{F_0} C = \frac{m\omega_0^2}{F_0} \frac{F_0}{\sqrt{m^2(\omega_0^2 - \omega^2)^2 + \omega^2 c^2}} = \frac{1}{\sqrt{\frac{m^2(\omega_0^2 - \omega^2)^2}{m^2\omega_0^4} + \frac{\omega^2 c^2}{m^2\omega_0^2}}}$$

$$\frac{m\omega_0^2}{F_0} C = \frac{mkC}{mF_0} = \frac{1}{\sqrt{\left[1 - \left(\frac{\omega}{\omega_0}\right)^2\right]^2 + \left(\frac{\omega}{\omega_0}\right)^2 \frac{c^2}{m^2\omega_0^2}}}$$

- Dimensionless amplitude depends on  $\omega/\omega_0$  and  $c^2/m^2\omega_0^2 = c^2/mk$
- Previous result:  $(\omega^2/\omega_0^2)_{\max} = 1 - c^2/m^2\omega_0^2$

California State University Northridge 40



### Summary

- General solutions for ODEs with order  $n \geq 2$  for constant coefficients only
  - Solutions are series of  $e^{\lambda_k x}$  terms where  $\lambda_k$  are solutions of algebraic equation
  - Special cases: double and complex roots
- Get general solution as  $y = y_H + y_p$ 
  - Use method of undetermined coefficients (simpler than variation of parameters) to find  $y_p$

California State University Northridge 42